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DOI:
10.1063/1.5020002

Document Version
Accepted author manuscript

Demixing, surface nematization, and competing adsorption in binary mixtures of hard rods and hard spheres under confinement

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(Dated: 20 March 2018)

A molecular simulation study of binary mixtures of hard spherocylinders (HSCs) and hard spheres (HSs) confined between two structureless hard walls is presented. The principal aim of the work is to understand the effect of the presence of hard spheres on the entropically-driven surface nematization of the hard rod-like particles at the walls. The mixtures are studied using a constant normal-pressure Monte Carlo algorithm. The surface adsorption at different compositions of hard spheres is examined in detail. At moderate hard-sphere concentrations preferential adsorption of the spheres at the wall is found. However, at moderate to high pressure (density), we observe a crossover in the adsorption behaviour with nematic layers of the rods forming at the walls leading to a local demixing of the system. The presence of the spherical particles is seen to destabilize the surface nematization of the rods, and the degree of demixing increases on increasing the HS concentration.

I. INTRODUCTION

Particle shape is one of the most important features governing the collective behaviour of colloidal suspensions[1,2]. As the shape of a particles deviates from spherical geometry, a rich phase behaviour emerges due to the additional orientational degrees of freedom giving rise to a variety of complex crystal, plastic crystal, and liquid crystals (LC) structures.[3–7] Colloidal particles are also attractive as model systems to study various physical phenomena due to the possibility of controlling the range, strength, and form of the interparticle interactions, even to the limit of designing interactions that are purely repulsive at short range, i.e., approaching the hard-core interaction limit[8]. In his pioneering work in 1949, Onsager[9] offered a successful explanation for the isotropic-nematic phase transition observed in uniaxial anisotropic particles such as thin rods modelled as hard spherocylinders (HSCs): cylinders of diameter D and length L capped at each end by hemispheres of diameter D. Onsager described the isotropic-nematic phase transition as a competition between the orientational entropy, which favours the stabilization of isotropic (Iso) phases, and the packing (free-volume) entropy which induces the alignment of the particles thus promoting the formation of nematic (Nem) phases. Onsager's second-virial theory provides a good description of rod-like particles in the limit of extreme shape anisotropies corresponding to $L/D \to \infty$ in the case of HSCs[10]. As the aspect ratio L/D of the particles is decreased, the theory becomes less reliable and more accurate methods such as higher-order density functional theories (DFTs)[11,12] and computer simulations[10,13] are required to accurately describe the ordering transitions.

The phase behaviour of non-spherical particles becomes even more complex in the presence of external potentials such as electromagnetic fields, gravity, and geometric confinement[14]. The behaviour of rod-like particles in contact with solid substrates modelled as hard structureless walls have been studied extensively[15–17]. The broken spatial symmetry along the normal direction to the wall induces additional phenomena, such as anchoring (see Ref.[16] for a review), in which the orientation of the particles at the wall is different to that in the bulk system; in some cases the extent of the surface orientation may be of a macroscopic dimension. The influence of the alignment of the particles at the wall on the isotropic-nematic transition has been studied theoretically using a variety of approaches including phenomenological Landau-de Gennes theory[18], mean-field DFT[19–21], and generalized Onsager theory[22–25]. A second-virial Onsager theory has been employed by van Roij *et al.*[26] to study confined rectangular rods in which the orientations of the particles are restricted to three possible directions (the Zwanzig model): a continuous uniaxial-biaxial nematic surface phase transition was found for an isotropic fluid in contact with a single planar hard wall, followed by wetting of the wall by a nematic film comprised of particles oriented parallel to the wall corresponding to homogeneous (planar) alignment. The appearance of the nematic film was found to occur before the phase transition to a bulk nematic phase away from the wall. A first-order capillary nematization transition was observed when the fluid was confined between two parallel hard walls with a capillary critical point for wall intersepa-

rations of about twice the length of the rods. Using a similar model, Aliabadi *et al.*[27] showed that the width of the nematic film diverges logarithmically as the density of the systems approaches the isotropic-nematic transition. The effect of confinement on the positional order and smectic layering of aligned hard cylinders has also been studied using the Onsager free-energy functional[28]. More recently, the surface induced phase transitions of semi-flexible polymer chains confined between two parallel walls have been studied using a self-consistent field theory[29]. Despite these efforts, an accurate theoretical description of liquid crystalline ordering near solid surfaces remains very challenging (see Ref.[30] for a recent review).

Computer simulation studies of various non-spherical particles either under confinement or in the presence of a solid substrate have been reported for a wide variety of model systems including hard spherocylinders[31–36], hard needles[25], hard ellipsoids[37,38], hard cut spheres[35,39], spherical caps[40], hard dimers[41], hard Gaussian overlap particles[42], Gay-Berne particles[43–46], and board-like Zwanzig models[26], as well as system of spherical particles decorated with an anisotropic Lennard-Jones potential[47], semiflexible polymer chains[48–51], and rod-like particles with chiral interactions[52,53]. Several types of surface-particle potentials and heterogeneities including surface roughness[54], softness[39], surface anchoring[17], competing walls[55], and spherical confinement[56] have also been examined in simulations of confined liquid crystals. In particular, the work of Mao *et al.*[32] and Dijkstra *et al.*[33] provides an excellent analysis of the adsorption, structure and orientation of hard spherocylinders at the surface of the wall. Mao *et al.*[32], for example, have reported Monte Carlo (MC) simulations of hard spherocylinders (with aspect ratios of $L/D = 10$ and 20) confined between two parallel hard structureless walls for states of relatively low density; the emphasis of their work was understanding the depletion forces induced by the walls, the surface adsorption, and the quantification of the surface tension for the isotropic fluid in contact with the wall. In their thorough simulation study, Dijkstra *et al.*[33] examine the behaviour of hard spherocylinders in contact with a single wall (allowing the thickness of the nematic film to diverge) investigating the surface adsorption and nematization of hard spherocylinders with an aspect ratio of $L/D = 15$. Simulation studies of the hard spherocylinders with $L/D = 10$ confined between two impenetrable parallel hard walls have been carried out to determine the profiles of the number density, nematic order parameter, degree of biaxiality, and normal and tangential components of the pressure tensor which allow one to obtain the fluid-wall interfacial tension of the system deep into the liquid-crystalline region[57,58]. Savenko and Dijkstra[59] also analysed the sedimentation and phase equilibria of hard spherocylinders on a planar hard wall observing the formation of nematic, smectic, and even crystal phases.

From the experimental perspective, liquid crystalline phases observed in suspensions of colloidal particles such as vandium pentoxide (V_2O_5)[60], Gibbsite ($Al(OH)_3$) platelets[61,62], carbon nanotubes[63], and some biological systems such as protein fibers[64], tobacco mosaic virus[65], *fd*-virus[66,67], polypeptide solutions[68,69], and DNA chains[70] offer convenient test beds for an assessment of the simple hard core models of mesogenic systems. The work by Galanis *et al.*[71] provides a very useful insight into the surface behaviour of granular rod-like particles (with aspect ratios of $L/D \sim 20$) for very thin layers of rods in a quasi-2D circular container. The number density profiles measured are in excellent agreement with previous findings from computer simulations. The influence of a flat wall on the surface anchoring of colloidal rods has been examined for aqueous suspensions of silica particles[72]. As with other colloidal systems of this type, the silica rods show a similar behavior to the athermal (purely repulsive) system and are of sufficiently low polydispersity to allow the formation of nematic and and smectic phases with increasing particle concentration. Good agreement is found with corresponding results obtained from computer simulations of hard spherocylinders[10,11,13,73–76]. This interesting work provides experimental confirmation that rod-like particles adopt a planar anchoring configuration in the vicinity of the surface. In this experimental analog of the hard-core system, the effect of the surface spans over tens of microns.

Beside the aforementioned studies dealing with one-component liquid-crystalline systems, there is a large body of work devoted to modelling and understanding the phase behaviour of athermal mixtures of mesogenic components including rod-rod[67,77–80], rod-sphere[81–91], rod-disc[92–99] and disc-disc[100,101] and disc-sphere[102] hard-core systems. The reader is directed to Reference 103 for a more detailed discussion. Although theoretical studies of binary mixtures of rod-like and spherical particles in the presence of structureless solid substrates have been reported[85,104], computer simulation studies of rod-sphere mixtures under confinement in the form of a slit pore are scarce[91].

It is the purpose of our current paper to fill this gap. Here, we study the adsorption behaviour of binary mixtures of hard spheres and hard spherocylinders confined by parallel hard wall using Monte Carlo simulation. This model system is entirely athermal and hence its properties are governed by purely entropic effects. In our previous work[91], we described the isotropic-nematic phase behaviour of the mixture in bulk. We now extend this study by assessing the effect of hard walls on formation of nematic films at conditions where only an isotropic phase is stable in the bulk. In particular, we examine the trade off between the stabilization of the nematic phase by presence of the wall and destabilizing effect of the hard spheres on the orientational order of the system.

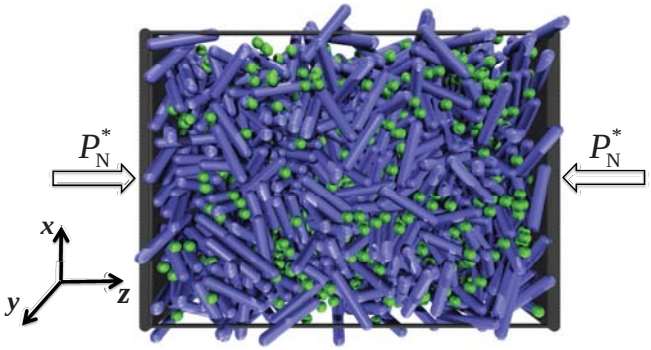

FIG. 1. Geometry and simulation set up used in our NP_NT Monte Carlo simulations to study binary mixtures of hard spherocylinders (blue) and hard spheres (green) confined between two hard walls. The parallel hard walls are placed along the z axis and the equilibrium (normal) pressure P_N is applied perpendicularly to the walls.

II. SIMULATION DETAILS

The methodology employed in our current work is similar to that described in a previous paper[91]. Binary mixtures of hard spherocylinders and hard spheres confined between two hard walls are studied using constant normal-pressure Monte Carlo simulation (NP_NT-MC), where N is the total number of particles, P_N is the normal pressure (directed perpendicular to the wall), and T is the absolute temperature. Strictly speaking, the surface area A and the global composition of the mixture should be included in the designation of the ensemble but we choose to retain the NP_NT abbreviation for conciseness, bearing in mind that the latter variables are also kept constant. Throughout our simulations, the number of hard spherocylinderss with an aspect ratio $L/D = 5$ is fixed at $N_{\rm HSC} = 1482$ while the number of hard spheres $N_{\rm HS}$, also of a diameter D, is varied to specify the hard-sphere mole fraction (composition) given by $x_{\rm HS} = N_{\rm HS}/N$ where $N = N_{\rm HS} + N_{\rm HSC}$.

The geometry of the simulation set up is shown in Figure 1. We consider a rectangular simulation box with standard Cartesian coordinates oriented along the box edges. Two parallel hard structureless walls are positioned at $z = 0$ and $z = L_z$ along the z axis and standard periodic boundary conditions are applied along the x and y directions. The volume of the system is allowed to fluctuate during the NP_NT-MC simulations by varying the dimension of the z axis (L_z), while the dimensions of the system along the x and y axes ($L_x = L_y = 25\,D$) are kept fixed. For systems with this planar symmetry the condition of mechanical equilibrium ($\nabla \cdot \mathbf{P} = 0$) requires that the normal component of the pressure tensor is constant throughout the sample, and as a consequence the normal component is also equivalent to the equilibrium pressure of the system. With $N_{\rm HSC}$ fixed, we may choose the following thermodynamic parameters to define a given system: the composition $x_{\rm HS}$, the normal pressure $P_{\rm N}$, and the surface area of the x-y plane ($A = L_xL_y = 625D$).

The $NP_{\rm N}T$-MC simulations are performed for 5×10^6 cycles to equilibrate the system and $5 - 8 \times 10^6$ cycles to accumulate ensemble the averages. Each MC cycle consists of N attempts to displace (and rotate in case of the hard spherocylinders) a randomly chosen molecule and one trial volume change in which the z dimension is scaled. The breaking of symmetry caused by the hard walls leads to inhomogeneous positional and orientational distributions of the particles along the z axis. In order to evaluate the one-body number density profile $\rho_i(z)$, for $i = \{\mathrm{HS}, \mathrm{HSC}\}$, the composition profile $x_i(z)$, and the nematic order parameter profile $S_2(z)$, the simulation box is divided into $n_{\rm bin}$ bins of equal width δz along the z direction. The density profile $\rho_i(z)$ is calculated as

$$\rho_i(z) = \frac{\langle N_i(z)\rangle D^3}{L_xL_y\delta z} \quad \text{for} \quad i = \mathrm{HS}, \mathrm{HSC}, \tag{1}$$

where $\langle N_i(z)\rangle$ represents the ensemble average of the local number of particles of component i at position z. Typically $n_{\rm bin} = 200$ bins are used for the calculations. The local composition profile $x_i(z)$ of the mixture is determined as

$$x_i(z) = \frac{\rho_i(z)}{\rho_{\rm HS}(z) + \rho_{\rm HSC}(z)} \quad \text{for} \quad i = \mathrm{HS}, \mathrm{HSC}. \tag{2}$$

Provided the system is sufficiently large, one expects that the structural and thermodynamic quantities determined from the central part of the box are consistent with the corresponding bulk limits. In particular, the density profiles $\rho_{\rm HSC}(z)$ and $\rho_{\rm HS}(z)$ are expected to reach the values of the corresponding bulk densities of $\rho_{\rm HSC,b}$ and $\rho_{\rm HS,b}$ far away from the wall. Having determined the bulk densities, the adsorption Γ_i of each component can be quantified from the following integral:

$$\Gamma_i = \frac{1}{D}\int_0^{L_z} [\rho_i(z) - \rho_{i,\mathrm{b}}]\mathrm{d}z \quad \text{for} \quad i = \mathrm{HS}, \mathrm{HSC} \tag{3}$$

It is important to note that in the case of our confined system the overall volume of the system includes the two regions inaccessible to the hard particles in layers of thickness $D/2$ close to the two walls.

The orientational order of the hard-spherocylindrical rods is quantified using the average of the second Legendre polynomial S_2[105] of relative orientation the principle axis of the particles with respect to the nematic director. The nematic order parameter profile $S_2(z)$ is obtained by determining the Saupe ordering tensor $\mathbf{Q}(j)$ in each bin j:

$$\mathbf{Q}(j) = \left\langle \frac{1}{2N_{\mathrm{HSC},j}} \sum_{i=1}^{N_{\mathrm{HSC},j}} (3\hat{\omega}_i \otimes \hat{\omega}_i - \mathbf{I}) \right\rangle \tag{4}$$

where $\hat{\omega}_i$ is the orientation of rod i, $N_{\mathrm{HSC},j}$ is the number of hard spherocylinders in bin j, and $\mathbf{I}$ is the unit tensor. On diagonalization of the $\mathbf{Q}(j)$ tensor[106], three eigenvalues are obtained and the largest value is defined as the

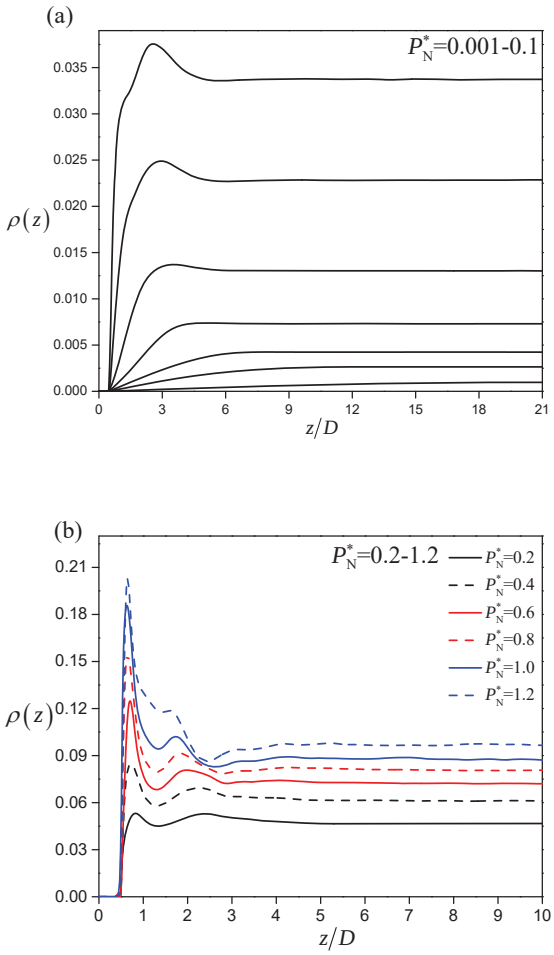

FIG. 2. Density profiles $\rho(z)$ for a system of pure $L/D = 5$ hard spherocylinders confined between parallel hard walls obtained from NP_NT-MC simulation along the normal direction to the wall. The curves correspond to the equilibrium (normal) pressures of (from bottom to top): (a) $P_N^* = [0.001, 0.003, 0.005, 0.01, 0.02, 0.05, 0.1]$; and (b) $P_N^* = [0.2 - 1.2]$ in increments of $\Delta P_N^* = 0.2$.

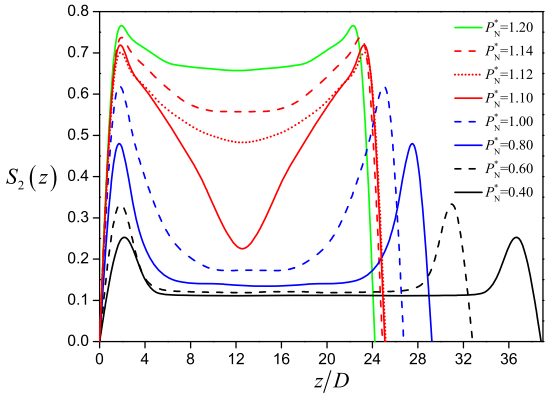

FIG. 3. Nematic order parameter profiles for a system of pure $L/D = 5$ hard spherocylinders confined between parallel hard walls obtained from NP_NT-MC simulation. The curves correspond to equilibrium (normal) pressures in the range $P_N^* = [0.4 - 1.2]$ (from bottom to top).

local nematic order parameter $S_2(z)$ associated with bin j. Some care should be taken with the calculation of the order parameter profile due to finite-size effects. Eppenga and Frenkel[107] have shown that the order parameter depends on the number of mesogenic particles, such that the system-size effect in the local order parameter is proportional to $1/(\sqrt{N_{\rm HSC}/n_{\rm bin}})$. If we consider $n_{\rm bin} = 200$ histogram bins, equivalent to the number of bins used in our calculations of the density profiles, the average number of the hard spherocylinders present in each bin is $(1482/200) \sim 7$ leading to a high system-size error of ~ 0.37 in the local order parameter. One can address this problem using a rescaling procedure for $S_2(z)$ in terms of $S_{2,\infty}(z)$ the infinite system[108], or simply by enlarging the simulation box at the cost of increasing the computational time. We opt instead to reduce the number of bins to $n_{\rm bins} = 20$, corresponding to a lower finite-size error in the calculated nematic order parameter profile of ~ 0.11.

Throughout our work the thermodynamic variables are expressed in dimensionless units: pressure $P_N^* = P_N D^3/(k_B T)$, number density $\rho = ND^3/V$, and adsorption $\Gamma^* = \Gamma D^2$. All length dimensions are given in units of D.

III. RESULTS AND DISCUSSION

A. Pure hard spherocylinders in planar confinement between hard walls

We first discuss our findings for the phase behaviour of pure hard spherocylinders with an aspect ration of $L/D = 5$ in planar confinement between parallel structureless hard walls over a wide range of equilibrium pressures (normal component of the pressure tensor) up to conditions where the bulk isotropic-nematic phase transition is found. The local density near the hard wall in the low-pressure range of $P_N^* = [0.001 - 0.1]$ is shown in Figure 2(a). At a pressure of $P_N^* \sim 0.02$ a peak in the density profile emerges at $z \sim 3D$, with the maximum of the peak becoming progressively more pronounced as the pressure is increased. The appearance of this peak is explained by the fact that for these very low density states, hard spherocylinders with an aspect ratio of $L/D = 5$ maintain their orientational freedom at $z \sim 3D$, which corresponds to half of the total length $L + D$ of the particles[31,32]. In this low-pressure regime, the wall is actually dried (dewetted) of the rod particles. The evolution of the density profiles at higher pressures, corresponding to the range $P_N^* = [0.2 - 1.2]$, is shown in

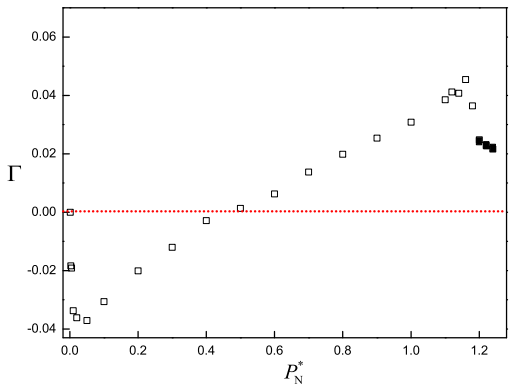

FIG. 4. Surface adsorption as a function of the equilibrium (normal) pressure P_N^* for a system of pure $L/D = 5$ hard spherocylinders confined between parallel hard walls obtained from NP_NT-MC simulation. The open squares correspond to bulk isotropic states, the filled squares to bulk nematic states, and the dashed black curve is drawn to guide the eye.

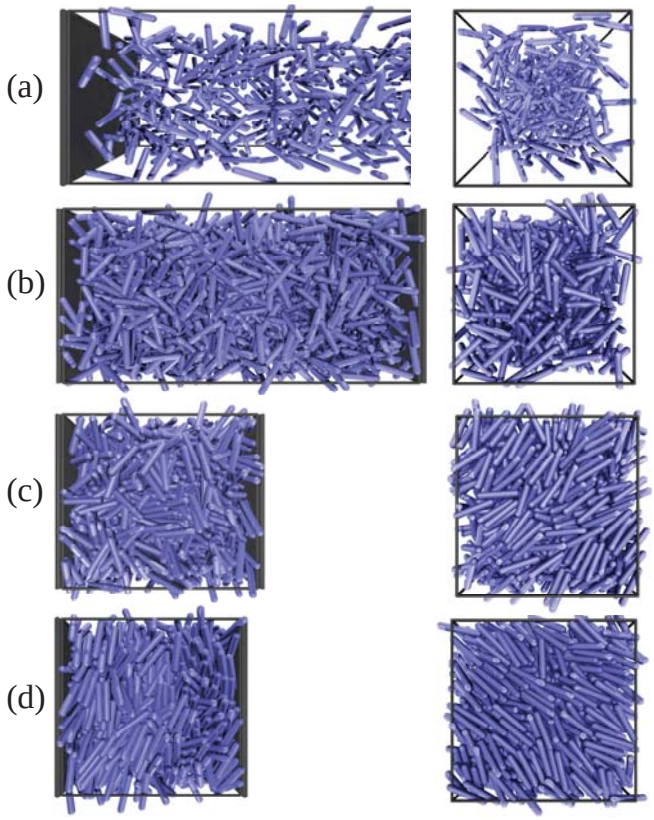

FIG. 5. Representative configurations for a system of pure $L/D = 5$ hard spherocylinders confined between parallel hard walls obtained from NP_NT-MC simulation at various equilibrium (normal) pressures: (a) $P_N^* = 0.02$; (b) $P_N^* = 0.20$; (c) $P_N^* = 0.90$; and (d) $P_N^* = 1.14$. The configurations are shown in the direction parallel to the hard walls (xy plane) on the left, and in the direction perpendicular to the hard walls (along the z direction) on the right.

Figure 2(b). The amplitude of the first peak at $z \sim 3D$ decreases while a new peak near $z \sim D/2$ emerges and quickly becomes the dominant feature of the density profile as P_N^* is increased. The peak near $z \sim D/2$ indicates an increasing adsorption of rods at the wall corresponding to planar anchoring in the first wetting layer. For this pressure interval a second wetting layer is also observed between $z \sim 3D/2$ and $\sim 5D/2$, and the maximum of this peak moves closer to the wall as the pressure is increased indicating that the adsorbed rods are parallel to the wall. The formation of the wetting layer appears to be continuous in this case. For strongly attractive walls, one would expect the layering transition near the wall to be first-order, followed by the bulk isotropic-nematic transition.

In order to get deeper insight into the structure of the hard spherocylinders near the wall, the local order parameter $S_2(z)$ is calculated as a function of the normal distance z (see Figure 3). We choose $S_2(z) < 0.4$ to represent a disordered state and $S_2(z) > 0.4$ to represent a local nematic-like structure in similar manner as for bulk phases[11]; though one would expect non-zero values of the nematic order parameter even for isotropic states due to finite-size effects, the choice is somewhat arbitrary. For a pressure of $P_N^* > 0.8$, the peak in $S_2(z)$ close to the wall in Figure 3 is associated with a local surface-induced nematization. As the pressure increases further, the amplitude of the peak also increases indicating an expected enhancement of the orientational ordering of the rods at the wall.

We can distinguish three density (pressure) regimes for the pure component hard spherocylinders near the hard wall. In the low-density regime, corresponding to the pressure range of $P_N^* = [0.001 - 0.01]$, the density profiles increase monotonically before reaching the bulk density plateau. This behaviour is expected since at low densities the hard rods maximize their orientational entropy when they are away from the repulsive wall. For moderate densities, corresponding to the pressure range of $P_N^* = [0.02 - 0.4]$, the interplay between the orientational entropy and packing effects gives rise to a non-monotonic behaviour of the density profile with a pronounced maximum at $\sim (L+D)/2 = 3D$ beyond which the rods are free to rotate. The third regime seen at higher bulk densities, corresponding to the pressure range of $P_N^* = [0.6 - 1.2]$, is characterized by surface nematization with the nematic director parallel to the wall. This surface wetting is indicated by the shift of the first maximum in the density profile to $z \sim D/2$. The second maximum located at $z \sim 2D$ indicates an effect of the orientation of the rods (S_2 is large in this region), in contrast with what is found for the hard-sphere fluid in which case the second maximum lies at $z \sim 3D/2$[109–111].

From Figure 3 we can also observe a marked growth in the nematic order parameter in the central part of the system which occurs between $P_N^* = 1.10$ and $P_N^* = 1.14$.

Although we cannot exclude that the nematization of the central part can (to a minor degree) be affected by capillary effects, we associate this orientational ordering with the bulk isotropic-nematic transition of the system; the corresponding values of the bulk densities for the coexisting isotropic and nematic states are $\rho^*_{\rm iso} = 0.0867$ and $\rho^*_{\rm nem} = 0.0941$, respectively. This result is consistent with our previously reported data[91] and also with the values from an earlier study[11] ($P^* = 1.19$, $\rho^*_{\rm iso} = 0.0914$ and $\rho^*_{\rm nem} = 0.0932$) obtained with isobaric-isothermal NPT-MC simulations for systems of pure hard spherocylinders with an aspect ratio of $L/D = 5$. The isotropic-nematic transition in the confined system is seen to occur at a slightly lower pressure compared to the bulk unconfined system, indicating a small degree of capillary stabilization.

The dependence of adsorption on the equilibrium (normal) pressure is shown in Figure 4. In the low pressure regime ($P^*_{\rm N} = 0.001$–0.08) the system is seen to primarily maximize its orientational entropy which results in the depletion of the rods particles from the vicinity of the wall. It is apparent from Figure 2(a) that for this low-pressure regime the density profiles significantly differ from the corresponding bulk density limit only in the close vicinity of the wall where the local density is almost zero; it is unlikely to accommodate a randomly oriented particle in this region. The only significant contribution to the adsorption in this region is proportional to $-\rho_b L_w$ where $L_w \sim (L + D)/2$ is the approximate dimension of the depleted region near the wall. The adsorption exhibits a minimum at $P^*_{\rm N} \sim 0.08$ beyond which we observe a near linear grow up to the IN transition. This can again be understood on the basis of our previous results. In this regime, the local surface nematization occurs which allows for surface enhancement a the contact density $\rho(D/2)$ which is proportional to P_N according to the contact theorem. Finally, the formation of the bulk nematic phase leads to an abrupt reduction in adsorption as a result of the increment of the bulk density.

We conclude the analysis of pure hard spherocylinders by discussing some representative snapshots of equilibrium configurations of selected states shown in Figure 5. It can clearly be seen that at the lowest pressure ($P^*_{\rm N} = 0.02.$), the wall tends to be relative dry of the rod particles, while a planar anchoring is noticeable at $P^*_{\rm N} = 0.20$. At even higher pressure ($P^*_{\rm N} = 0.90$), the system is seen to exhibit surface nematization before experiencing a bulk isotropic-nematic transition at $P^*_{\rm N} \sim 1.14$.

B. Binary mixtures of hard spherocylinders and hard spheres in planar confinement between hard walls

We are now in a position to study the influence of hard spheres on the surface behavior of binary mixtures of hard spherocylinders and hard spheres. The case of the equimolar mixture ($x_{\rm HS} = 0.5$) is considered first. Density profiles of both species over the pressure range of $P^*_{\rm N} = [0.02 - 0.1]$ are shown in Figure 6. As observed in the system of pure hard spherocylinders, these low-pressure isotropic states are characterized by a depletion of rods from the wall that maximizes their orientation entropy. In turn this creates an available volume near the wall that is free free for occupation by the smaller hard-sphere particles. In view of the isotropic character

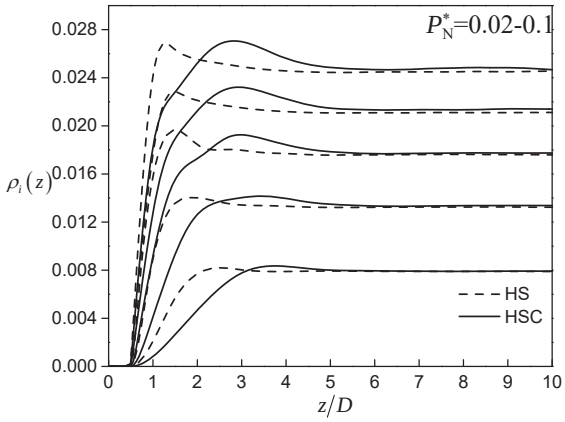

FIG. 6. Density profiles $\rho_i(z)$ of a binary equimolar mixture ($x_{\rm HS} = 0.5$) of $L/D = 5$ hard spherocylinders (HSC, continuous curves) and hard spheres (HS, dashed curves) confined between parallel hard walls obtained from NP_NT-MC simulation. The various curves correspond to states with different equilibrium (normal) pressures $P^*_{\rm N}$: from bottom to top, $P^*_{\rm N} = [0.02 - 0.1]$ with increments of $\Delta P^*_{\rm N} = 0.02$.

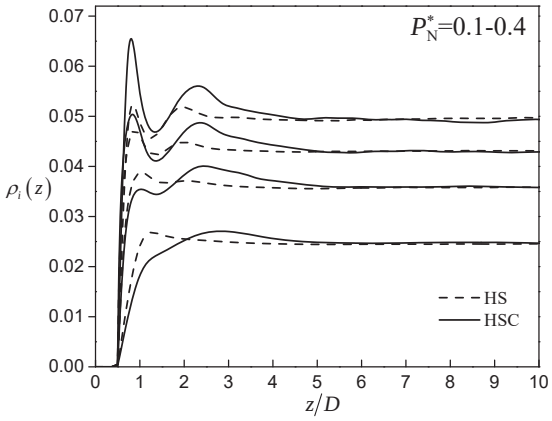

FIG. 7. Density profiles $\rho_i(z)$ of a binary equimolar mixture ($x_{\rm HS} = 0.5$) of $L/D = 5$ hard spherocylinders (HSC, continuous curves) and hard spheres (HS, dashed curves) confined between parallel hard walls obtained from NP_NT-MC simulation. The various curves correspond to states for different equilibrium (normal) pressures $P^*_{\rm N}$: bottom to top, $P^*_{\rm N} = [0.1, 0.2, 0.3, 0.4]$.

of the lower density states, the HSC components behave essentially like hard spheres with an effective diameter of $\sim (L+D)/2$. Consequently, the hard spheres are preferentially adsorbed at the wall and the corresponding density profiles exhibit a weak peak at $z \sim D$, while a peak in the density profiles of hard spherocylinders develops at $z \sim 3D$. The density profiles for the intermediate pressure range of $P_{\rm N}^* = [0.1 - 0.4]$ is shown in Figure 7. As the pressure is increased, a new peak adjacent to the wall ($z \sim D/2$) develops in the density profile of the hard spherocylinders which exceeds the one for hard spheres for pressures $P_{\rm N}^* > 0.2$ and can be attributed to the onset of the surface nematization and planar anchoring. As the pressure is further increased, the second peak in the density profile for the rods moves towards the wall from $z \sim 3D$ to $z \sim 2D$ due to propagation of the nematic ordering away from the wall; the density profiles for the hard spherocylinders is now seen to exhibit oscillations with a periodicity of D rather than $(L+D)/2$. The enhancement of surface nematization by the rods leads to the spheres being pushed away from the wall, resulting in a reduction of the hard-sphere density near the wall reflected by the progressively weaker amplitude of the first peak.

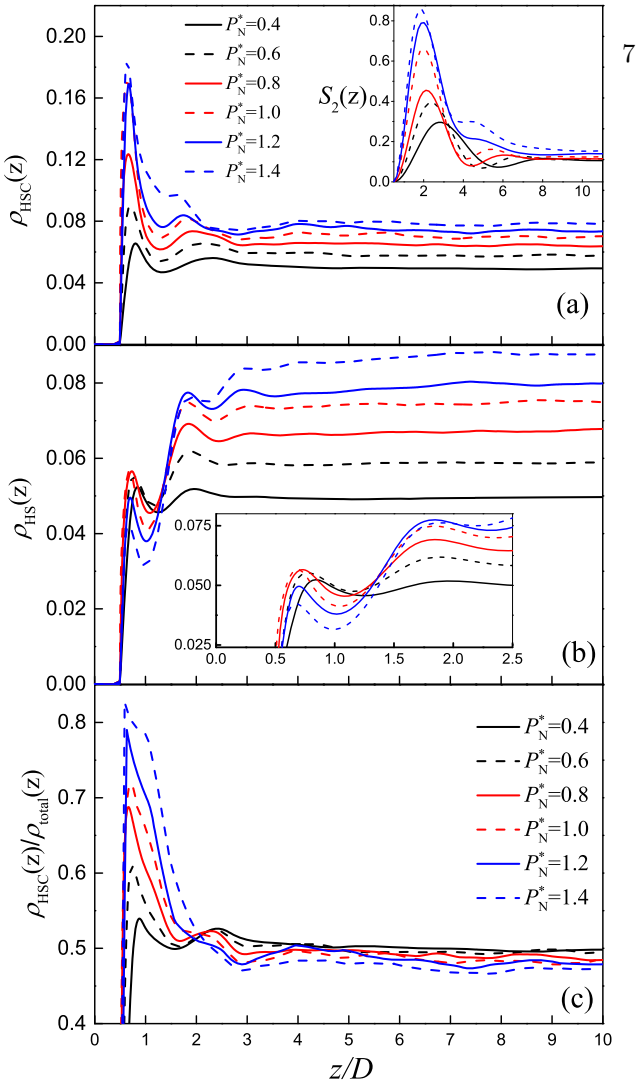

FIG. 8. Density profiles $\rho_i(z)$ for (a) $L/D = 5$ hard spherocylinders and (b) hard spheres in a binary equimolar mixture ($x_{\rm HS} = 0.5$) confined between parallel hard walls obtained from NP_NT-MC simulation. The various curves correspond to states for different equilibrium (normal) pressures $P_{\rm N}^*$: from bottom to top, $P_{\rm N}^* = [0.4 - 1.4]$. The nematic order parameter profiles $S_2(z)$ of the hard spherocylinders is shown in the inset of (a). The behaviour of the density profiles for hard spheres near a hard wall is highlighted in the inset of (b). (c) The corresponding concentration profiles $x_{\rm HSC}(z) = \rho_{\rm HSC}(z)/\rho_{\rm total}(z)$.

The behaviour of the equimolar mixture of hard spherocylinders and hard spheres at higher equilibrium (normal) pressures in the range $P_{\rm N}^* = [0.4 - 1.4]$ is shown in Figure 8. It is clear from the density profiles that higher pressures enhance the orientational ordering of the rods near the wall, which is also reflected in the behavior of the nematic order parameter seen to increase significantly near the wall. In this high-pressure regime we observe an onset of a surface nematization, although at a somewhat higher pressure ($P_{\rm N}^* \sim 1.0$) than in the case of the pure hard-spherocylinder system ($P_{\rm N}^* \sim 0.7$), demonstrating that the presence of hard spheres destabilizes the nematic ordering of the rods. The surface nematization leads to even stronger depletion of the hard spheres from

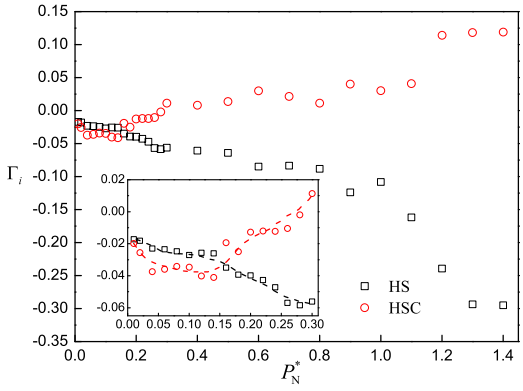

FIG. 9. Surface adsorption Γ_i $(i = \mathrm{HSC}, \mathrm{HS})$ of a binary equimolar mixture ($x_{\mathrm{HS}} = 0.5$) of $L/D = 5$ hard spherocylinders (HSC, circles) and hard spheres (HS, squares) confined between parallel hard walls as a function of the equilibrium (normal) pressure P_{N}^* obtained from NP_NT-MC simulation. The competing adsorption between the rods and spheres is highlighted in the inset. Dashed curves are drawn to guide the eye.

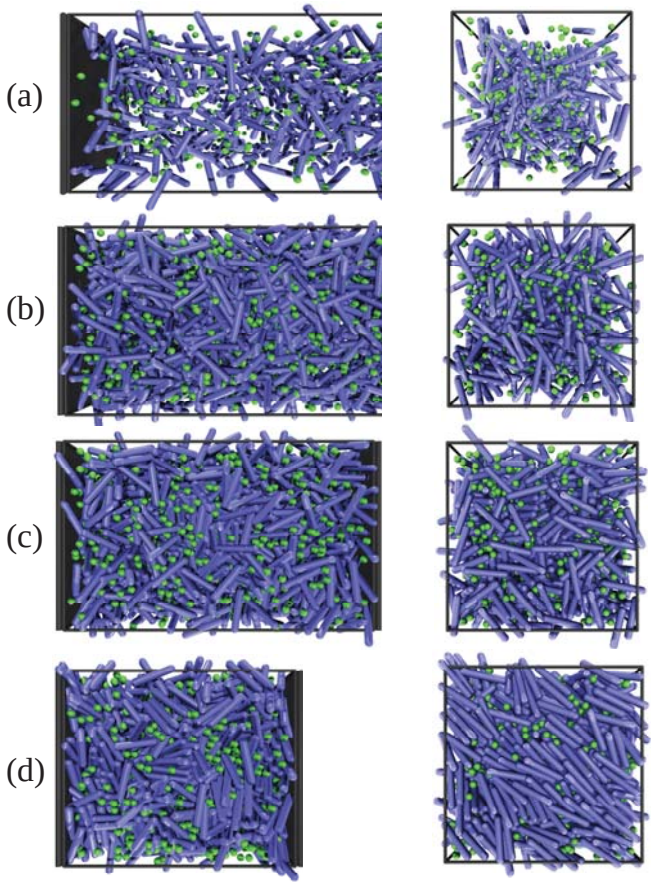

FIG. 10. Representative configurations for a binary equimolar mixture ($x_{\mathrm{HS}} = 0.5$) of $L/D = 5$ hard spherocylinders and hard spheres confined between parallel hard walls obtained from NP_NT-MC simulation at various equilibrium (normal) pressures: (a) $P_{\mathrm{N}}^* = 0.04$; (b) $P_{\mathrm{N}}^* = 0.26$; (c) $P_{\mathrm{N}}^* = 0.60$; and (d) $P_{\mathrm{N}}^* = 1.40$. The configurations are shown in the direction parallel to the hard wall (xy plane) on the left, and in the direction perpendicular to the hard wall (along the z direction) on the right.

the wall than in the low-pressure regime, which leads to local demixing of the fluid.

The behaviour of the binary mixture can also be analysed from the surface adsorption of the hard spherocylinders (Γ_{HSC}) and hard spheres (Γ_{HS}) calculated using Eq.3 depicted in Figure 9. At low pressures, the adsorption is negative for both components, with the adsorption of hard spheres just slightly higher than that of the hard spherocylinders. However, a crossover in adsorption is observed at a pressure of $P_{\mathrm{N}}^* \sim 0.16$ beyond which the rods are preferentially adsorbed. This behaviour is a consequence of the spheres being excluded from the region close to the wall due to the reorientation of the rods forming the first nematic layer. As the pressure is further increased, the preferential adsorption of hard spherocylinders becomes more evident leading eventually to a local demixing of the mixture. Representative snapshots of equilibrium configurations for equilibrium (normal) pressures ranging from the low-density isotropic states to the high-density nematic states are shown in Figure 10. The planar configuration of the rods in the high density state is clearly apparent.

It has been shown previously[88] that a presence of spherical particles in the system of rod-like particles destabilize the formation of the bulk nematic phase. Here, we analyze the impact of the presence of hard spheres on a formation of nematic films near a hard wall in binary mixtures of hard spherocylinders and hard spheres with different compositions. As shown in Figure 11 for mixtures at a fixed equilibrium (normal) pressure of $P_{\mathrm{N}}^* = 1.0$ with compositions of $x_{\mathrm{HS}} = 0, 0.1, 0.2,$ and 0.5, thick nematic films adsorb at the wall. The thickness and the orientational order of the nematic layer is seen to decrease as the composition of spheres is decreased. We can, therefore, conclude that not only the bulk isotropic-nematic transition but also the surface nematization is destabilized by the presence of hard spheres.

Based on the previous findings one might expect the presence of high concentrations of hard spheres to weaken the preferential adsorption of rods in favour of spheres. This is, however, not the case as inferred from the dependence of the surface adsorption on the hard-sphere composition presented in Figure 12. Here, we introduce the quantity $\Delta_{\mathrm{W}} = \Gamma_{\mathrm{HSC}} - \Gamma_{\mathrm{HS}}$ characterizing the relative adsorption of the hard spherocylinders with respect to that of the hard spheres. It is apparent that as the hard-sphere concentration is increased the adsorption of the hard spherocylinders is largely unaffected while the adsorption of the hard spheres decreases rather dramatically which is a consequence of depletion of the spheres

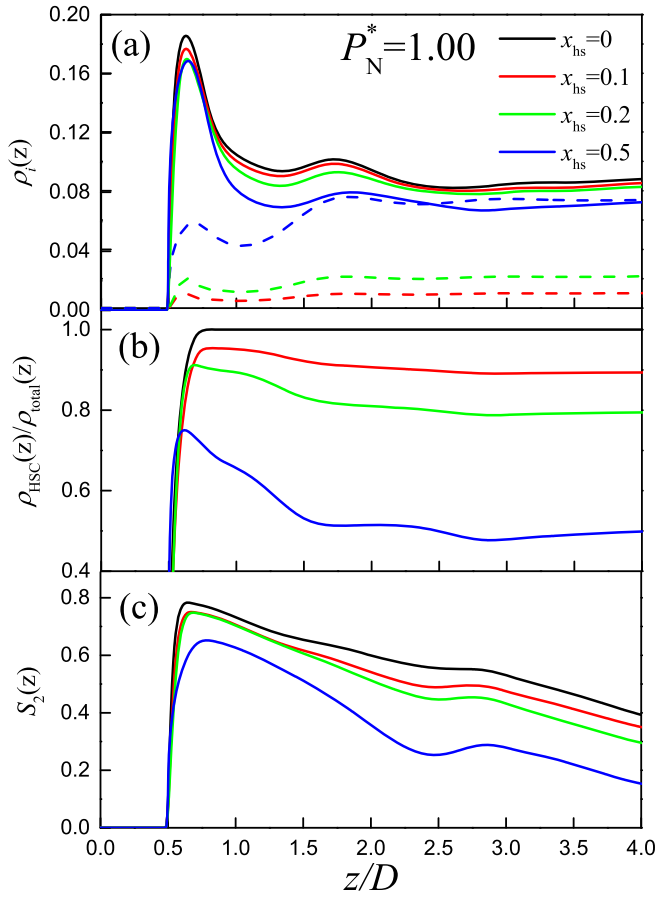

FIG. 11. (a) Density profiles $\rho_i(z)$, (b) concentration profiles $x_{\rm HSC}(z) = \rho_{\rm HSC}(z)/\rho_{\rm total}(z)$, and (c) nematic order parameter profiles $S_2(z)$ for mixtures of $L/D = 5$ hard spherocylinders and hard spheres confined between parallel hard walls obtained from NP_NT-MC simulation with varying overall hard-sphere composition $x_{\rm HS}$ at a fixed equilibrium (normal) pressure of $P_{\rm N}^* = 1.0$. The continuous curves in (a) represent the density profiles of the hard spherocylinders and the dashed curves are those for the hard spheres.

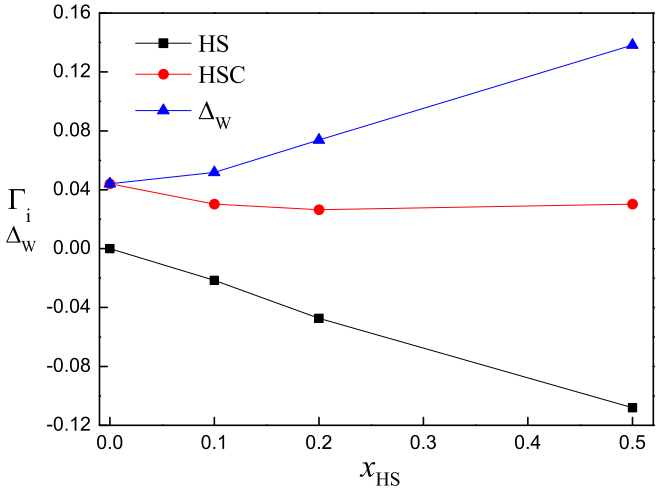

FIG. 12. Dependence of surface adsorption on the overall hard-sphere composition $x_{\rm HS}$ for mixtures of $L/D = 5$ hard spherocylinders and hard spheres confined between parallel hard walls obtained from NP_NT-MC simulation at a fixed equilibrium (normal) pressure of $P_{\rm N}^* = 1.0$. The trend for the differential adsorption $\Delta_{\rm W} = \Gamma_{\rm HSC} - \Gamma_{\rm HSC}$ is also included.

from the wall due to surface induced nematic ordering of the rods. The extent of local demixing near the wall therefore becomes stronger as the concentration of the hard spheres in the mixture is increased. For low concentrations of hard spheres, the effect of the presence of hard spheres is insignificant in terms of adsorption of hard spherocylinders in the nematic layer since the hard spheres are depleted from the wall in the high-pressure regime. It is only when $x_{hs} \sim 0.5$ that the presence of hard spheres can influence the order parameter appreciably.

IV. CONCLUSIONS

We have studied structure, orientational ordering and phase behaviour of pure hard spherocylinders and of binary mixtures of hard spherocylinders and hard spheres confined between parallel hard walls using constant normal pressure MC simulations. The aspect ratio of the hard spherocylinders considered is $L/D = 5$ and the hard-sphere diameter is taken to be the same as the cylinder diamater D. States up to the bulk isotropic-nematic transition are examined.

Starting with surface properties of pure rods, we find that at low-pressure (low-density) states the system is fully isotropic resulting in a depletion of the particles from the hard wall in order to maximize the (dominant) contribution to the orientational entropy. At higher pressures, packing effects prevail and the rods adsorb at the wall with a near-linear dependence of the adsorption with pressure. This process is accompanied by a surface nematization with the nematic director oriented parallel to the wall and the induced nematic film growing continuously up to the bulk isotropic-nematic transition.

The main objective of our study is a detailed examination of the effect of the surface on the properties of binary mixtures of rod-like and spherical particles. Here, the competition between the orientational entropy and packing effects near the wall leads to a local demixing of the mixture. At low pressures (densities) we observe a preferential adsorption of hard spheres that fill the free volume left by the rods near the wall from which the rods are depleted due to orientational entropy effects. This effect is, however, quite mild. At higher pressures, a crossover in the preferential surface adsorption occurs beyond which the local demixing near the wall is seen to increase with the pressure. In this regime, the rod particles adsorb at the wall to form a nematic film the width of which increases continuously as the isotropic-nematic transition is approached. The process is accompanied by an increase in the nematic order parameter and deple-

tion of the hard-sphere particles from the wall which in turn leads to local demixing. This process is continuous as we only consider states (pressures) corresponding to bulk isotropic phases. Sudden changes in the structure of the fluid are expected for even higher pressures which exceed the isotropic-nematic transition, as is observed in Figure 4 for the pure component hard-spherocylinder system. Overall, however, one can conclude that the presence of hard spheres is found to destabilize the surface nematization, and an increase in the hard-sphere concentration enhances demixing.

In our current work we focus exclusively on isotropic and nematic states. Smectic order of rod particles in confinement[28] and layering in rod-sphere mixtures[112] are examples of other surface induced structures occurring at higher pressures. A feature which has been omitted in our study is an analysis of the expected biaxiality and of the rod-like particles close to wall and the fluid-wall interfacial tension[33,57,58]. The method adopted in our current study to characterize the spatial distribution of the order parameter tensor is not sufficiently accurate to compute the biaxiality of HSCs induced by the surface. We postpone this to future work, and we also plan to use advanced DFT methodologies[12,85,113] to predict the surface behaviour of mixtures of rods and spheres including a detailed comparison with simulation.

ACKNOWLEDGMENTS

LW thanks the Department for Business Innovation and Skills of the UK and China Scholarship Council for funding a PhD studentship. The MC simulations were performed using the High Performance Computing service provided by Imperial College London. AM acknowledges support from the Czech Science Foundation, project 16-12291S. Funding to the Molecular Systems Engineering Group from the Engineering and Physical Sciences Research Council (EPSRC) of the UK (grants GR/T17595, GR/N35991, EP/E016340, and EP/J014958), the Joint Research Equipment Initiative (JREI) (GR/M94426), and the Royal Society-Wolfson Foundation refurbishment scheme is also gratefully acknowledged.

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